FPLO 14.00-49 / enhanced LO basis

name and version of the code: FPLO 14.00-49 type of basis set: numerical atom-centered local orbitals method: all-electron

GENERAL INFORMATION

exchange-correlation functional	PBE		
relativistic scheme	core and valence scalar relativistic		
	(Koelling-Harmon)		
assignment of core / valence states	see Section additional comments and table		
basis set size	enhanced (see below): 21-56 basis orbitals		
	(typical basis set size of 35)		
k-mesh density	see table (number of k-points in the full 1st		
	Brillouin zone of the primitive cell, $\# k$)		
reciprocal-space integration method	linear tetrahedron method		
METHOD-SPECIFIC INFORMATION			
numerical settings	all settings are default settings		
	except for the basis and k -mesh		

(see below and table).

ADDITIONAL COMMENTS

We enhanced the default basis according to the following scheme. The core and semi-core orbitals stay untouched. A double valence basis orbital (e.g. 3d4d) becomes a triple basis orbital (e.g. 3d4d5d) with the charge parameter $Q_3 = Q_2 + 2$ and compression parameter $P_3 = \max(0.85, P_2)$. A single valence basis orbital becomes a double basis orbital with $Q_2 = Q_1 + 2$ and $P_2 = \max(0.85, P_1)$. An additional f-orbital is added with Q = 4 and P = 1. For H and He additionally a single d-orbital (Q = 5, P = 1) is added to the default basis. In the table below, the basis set is denoted in the following way: semi-core orbitals are separated by a /, Dnl means double basis orbitals, e.g. D3p = 3p4p, Tnl means triple basis orbitals, e.g. T3p = 3p4p5p. The additional nominal 5f orbital for Lu is of course not identical to the 5f part of its T4f basis states but rather an effective 7f state. Ultra soft elements require a (non default) fixed compact support radius (as was used in the FPLO/T+F+s set of calculations). For this reason some of those elements (Xe, Rn, Hg) are excluded from the tables. The use of the linear tetrahedron method allows to keep the relatively small default k-mesh, except for the cases C, Al, Ag, where we used a higher k-point number for testing reasons.

REFERENCES

code

[1] K. Koepernik and H. Eschrig, Phys. Rev. B 59, 1743 (1999)

[2] www.fplo.de

scalar relativity

[3] D. D. Koelling and B. N. Harmon, J. Phys. C: Solid State 10, 3107–3114 (1977).

reciprocal-space integration

[4] G. Lehmann and M. Taut, Phys. Status Solidi B 54, 469–477 (1972).

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Table I. Calculation settings and results per element: k-point mesh in the full 1st Brillouin zone of the primitive cell *kpts* and number of irreducible k-points # k, valence, equilibrium volume per atom V_0 , bulk modulus B_0 , pressure derivative of the bulk modulus B_1 .

	knts [-]	# k [_]	semi-core/valence	Vo [Å ³ /atom]	B _o [GPa]	B ₁ [_]
н	$\frac{\kappa \rho \iota s}{12 \times 12 \times 12}$	$\frac{\# \kappa []}{1.728}$	/ T1 e D2n Af 3d		$\frac{D_0 \left[01 a \right]}{10.245}$	$\frac{D_{1}}{2612}$
Ηο	$12 \times 12 \times 12$ $19 \times 19 \times 19$	1720 1728	/ T1s D2p + f 3d	17.421	0.836	6 491
Li	$12 \times 12 \times 12$ $19 \times 19 \times 19$	1720 1728	$1e^{-113}D2p + 5u^{-1}$	20 302	13721	31/9
Bo	$12 \times 12 \times 12$ $19 \times 19 \times 19$	1720 1728	13 / 123 12p D3a 4f 1e / T2e T2p D3d Af	7 911	10.721 123 155	3.142
B	$12 \times 12 \times 12$ $19 \times 19 \times 19$	1720	13 / 123 12p D3a 4f 1e / T2e T2p D3d 4f	7.511	235,066	3 464
C	$12 \times 12 \times 12$ $12 \times 10 \times 30$	1 1 20	13 / 123 12p D3a 4f 1e / T2e T2p D3d 4f	11 659	205.900 207.885	3.404 3.579
N	$12 \times 12 \times 50$ $12 \times 12 \times 12$	4520 1728	13 / 123 12p D3a 4f 1e / T2e T2p D3d 4f	28.870	53 512	3.012 3.756
$\hat{\mathbf{O}}$	$12 \times 12 \times 12$ $12 \times 12 \times 12$	1720 1728	15 / 125 12p D3d 4f 1e / T2e T2p D3d 4f	18 605	40.733	3.844
С F	$12 \times 12 \times 12$ $12 \times 12 \times 12$	1720 1728	15 / 125 12p D3d 4f 1e / T2e T2p D3d 4f	10.030	49.100	0.044 4 041
r No	$12 \times 12 \times 12$ $12 \times 12 \times 12$	1720 1728	13 / 123 12p D3u 4j 1e / T2e T2p D3d 4f	24 480	1 991	$\frac{4.041}{7.193}$
No	$12 \times 12 \times 12$ $19 \times 19 \times 19$	1720 1728	2e 2n / T3e T3n D3d Af	37 170	7.221	3 670
Mo	$12 \times 12 \times 12$ $12 \times 12 \times 12$	1720 1728	2s 2p / 10s 10p D0a 4f 2s 2n / T3s T3n D3d 4f	22 936	35 882	4 141
	$12 \times 12 \times 12$ $30 \times 30 \times 30$	27 000	2s 2p / 10s 10p D0a 4f 2s 2n / T3s T3n D3d 4f	16 488	77.482	4 593
Si	$10 \times 10 \times 10$	1728	23 2p / 133 13p D3a 4f 2e 2n / T3e T3n D3d 4f	20.483	88 280	4.000
P	$12 \times 12 \times 12$ $12 \times 12 \times 12$	1720 1728	2s 2p / 10s 10p D0a 4f 2s 2n / T3s T3n D3d 4f	20.405	67 764	4 332
S	$12 \times 12 \times 12$ $19 \times 19 \times 19$	1720 1728	23 2p / 133 13p D3a 4f 2e 2n / T3e T3n D3d 4f	17 260	84 276	4.002
Cl	$12 \times 12 \times 12$ $19 \times 19 \times 19$	1720 1728	23 2p / 133 13p D3a 4f 2e 2n / T3e T3n D3d 4f	30 134	18579	4.123
Δr	$12 \times 12 \times 12$ $19 \times 19 \times 19$	1720 1728	23 2p / 133 13p D3a 4f 2e 2n / T3e T3n D3d 4f	52 686	0 719	4.403 8 102
K	$12 \times 12 \times 12$ $12 \times 12 \times 12$	1720 1728	23 2p / 133 13p D3a 4f 3s 3n / T4s D4n T3d 4f	73 926	3527	4.289
Ca	$12 \times 12 \times 12$ $12 \times 12 \times 12$	1720 1728	3s 3n / T4s D4n T3d 4f	42 320	17.476	2.505
Sc	$12 \times 12 \times 12$ $12 \times 12 \times 12$	1720 1728	3s 3n / T4s T3d D4n 4f	24 618	54 688	$\frac{2.000}{3.413}$
Ti	$12 \times 12 \times 12$ $19 \times 19 \times 19$	1720 1728	$3e^{3n}/T4e^{T3d}D4n^{4f}$	17 306	111 947	3 551
V	$12 \times 12 \times 12$ $19 \times 19 \times 19$	1720 1728	$3e^{3n}/T4e^{T3d}D4n^{4f}$		181 646	3 880
Čr	$12 \times 12 \times 12$ $12 \times 12 \times 12$	1720 1728	3s 3p / T4s T3d D4p 4f 3s 3n / T4s T3d D4n 4f	11 785	181.040 184.253	$\frac{5.000}{7.314}$
Mn	$12 \times 12 \times 12$ $19 \times 19 \times 19$	1720 1728	$3e^{3n}/T4e^{T3d}D4n^{4f}$	11.765	104.200 100.527	8 437
Fo	$12 \times 12 \times 12$ $19 \times 19 \times 19$	1720 1728	$3e^{3n}/T4e^{T3d}D4n^{4f}$	11 350	100.527	5 356
	$12 \times 12 \times 12$ $19 \times 19 \times 19$	1720 1728	$3e^{3n}/T4e^{T3d}D4n^{4f}$	10.878	$216\ 807$	4.965
Ni	$12 \times 12 \times 12$ $12 \times 12 \times 12$	1720 1728	3s 3n / T4s T3d D4n 4f	10.010	199.051	4.900
Cu	$12 \times 12 \times 12$ $12 \times 12 \times 12$	1720 1728	3s 3p / T4s T3d D4p 4f 3s 3n / T4s T3d D4n 4f	11 974	140 348	4.372 5.146
Zn	$12 \times 12 \times 12$ $12 \times 12 \times 12$	1728	3s 3n / T4s T3d D4n 4f	15 207	75 445	5.292
Ga	$12 \times 12 \times 12$ $12 \times 12 \times 12$	1728	3s 3n 3d / T4s T4n D4d 4f	20.383	48 761	5 182
Ge	$12 \times 12 \times 12$ $12 \times 12 \times 12$	1728	3s 3n 3d / T4s T4n D4d 4f	23.924	58 958	4 915
As	$12 \times 12 \times 12$ $12 \times 12 \times 12$	1728	3s 3n 3d / T4s T4n D4d 4f	22.633	67.560	4 039
Se	$12 \times 12 \times 12$ $12 \times 12 \times 12$	1720 1728	3s 3n 3d / T4s T4n D4d 4f	29.856	46 692	4.005
Br	$12 \times 12 \times 12$ $12 \times 12 \times 12$	1720 1728	3s 3n 3d / T4s T4n D4d 4f	39.636	$\frac{40.052}{22.145}$	4 752
Kr	$12 \times 12 \times 12$ $12 \times 12 \times 12$	1728	3s 3n 3d / T4s T4n D4d 4f	67 564	0.635	0.529
Rh	$12 \times 12 \times 12$ $12 \times 12 \times 12$	1728	4s 4n / T5s D5n T4d 4f	90.955	2.805	6.020
Sr	$12 \times 12 \times 12$ $12 \times 12 \times 12$	1728	4s 4n / T5s D5n T4d 4f	54 443	11,700	4.070
Y	$12 \times 12 \times 12$ $12 \times 12 \times 12$	1 728	4s 4n / T5s T4d D5n 4f	32.862	41 364	3525
Zr	$12 \times 12 \times 12$ $12 \times 12 \times 12$	1728	4s 4n / T5s T4d D5n 4f	23.403	94.148	3.428
Nb	$12 \times 12 \times 12$ $12 \times 12 \times 12$	1728	4s 4n / T5s T4d D5n 4f	18.117	169.586	3.694
Mo	$12 \times 12 \times 12$ $12 \times 12 \times 12$	1728	4s 4p / T5s T4d D5p 4f	15.806	259,205	4.263
Tc	$12 \times 12 \times 12$ $12 \times 12 \times 12$	1728	4s 4n / T5s T4d D5n 4f	14.467	297.489	4.445
Ru	$12 \times 12 \times 12$ $12 \times 12 \times 12$	1728	4s 4p / T5s T4d D5p 4f	13.793	$\frac{200100}{310.576}$	4.937
Rh	$12 \times 12 \times 12$ $12 \times 12 \times 12$	1728	4s 4p / T5s T4d D5p 4f	14.078	255.504	5.197
Pd	$12 \times 12 \times 12$	1728	4s 4p / T5s T4d D5p 4f	15.350	166.938	5.306
Ag	$30 \times 30 \times 30$	27000	4s 4p / T5s T4d D5p 4f	17.883	90.451	5.784
Cď	$12 \times 12 \times 12$	1728	4s 4p / T5s T4d D5p 4f	22.835	43.273	7.811
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FPLO/T+F

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In	$12 \times 12 \times 12$	1728	$4s \ 4p \ 4d \ / \ T5s \ D5d \ T5p \ 4f$	27.588	35.164	5.243
Sn	$12 \times 12 \times 12$	1728	$4s \ 4p \ 4d \ / \ T5s \ D5d \ T5p \ 4f$	36.922	35.119	4.834
Sb	$12 \times 12 \times 12$	1728	$4s \ 4p \ 4d \ / \ T5s \ D5d \ T5p \ 4f$	31.824	50.010	4.952
Te	$12 \times 12 \times 12$	1728	$4s \ 4p \ 4d \ / \ T5s \ D5d \ T5p \ 4f$	35.169	45.240	4.734
Ι	$12 \times 12 \times 12$	1728	$4s \ 4p \ 4d \ / \ T5s \ D5d \ T5p \ 4f$	50.976	18.078	3.423
\mathbf{Cs}	$12 \times 12 \times 12$	1728	5s 5p / T6s T5d D6p 5f	120.111	3.015	-1.820
Ba	$12 \times 12 \times 12$	1728	5s 5p / T6s D5d D6p 4f	63.901	6.052	6.146
Lu	$12 \times 12 \times 12$	1728	5s 5p / T6s T5d D6p T4f 5f	29.183	44.303	1.445
Hf	$12 \times 12 \times 12$	1728	$4f \; 5s \; 5p \; / \; T6s \; T5d \; D6p \; 5f$	22.584	106.895	2.931
Ta	$12 \times 12 \times 12$	1728	4f 5s 5p / T6s T5d D6p 5f	18.279	192.499	4.046
W	$12 \times 12 \times 12$	1728	4f 5s 5p / T6s T5d D6p 5f	16.178	301.300	4.285
Re	$12 \times 12 \times 12$	1728	4f 5s 5p / T6s T5d D6p 5f	14.994	352.329	4.370
Os	$12 \times 12 \times 12$	1728	4f 5s 5p / T6s T5d D6p 5f	14.314	389.219	5.053
Ir	$12 \times 12 \times 12$	1728	4f 5s 5p / T6s T5d D6p 5f	14.532	342.719	5.373
Pt	$12 \times 12 \times 12$	1728	$5s \ 5p \ / \ \mathrm{T}6s \ \mathrm{T}5d \ \mathrm{D}6p \ 5f$	15.691	254.342	4.624
Au	$12 \times 12 \times 12$	1728	$5s \ 5p \ / \ \mathrm{T6}s \ \mathrm{T5}d \ \mathrm{D6}p \ 5f$	18.021	138.071	4.300
Tl	$12 \times 12 \times 12$	1728	$5s\ 5p\ 5d\ /\ {\rm T6}s\ {\rm D6}d\ {\rm T6}p\ 5f$	31.889	24.827	-0.475
Pb	$12 \times 12 \times 12$	1728	$5s\ 5p\ 5d\ /\ {\rm T6}s\ {\rm D6}d\ {\rm T6}p\ 5f$	31.972	43.115	7.784
Bi	$12 \times 12 \times 12$	1728	$5s\ 5p\ 5d\ /\ {\rm T6}s\ {\rm D6}d\ {\rm T6}p\ 5f$	36.734	43.808	6.951
Ро	$12\times12\times12$	1728	$5s\ 5p\ 5d$ / T6s D6d T6p $5f$	37.458	45.587	5.567